Supplementary Information for

Direct regeneration of degraded lithium-ion battery cathodes with a multifunctional organic lithium salt

Guanjun Ji^{1,2#}, Junxiong Wang^{1,2#}, Zheng Liang^{2*}, Kai Jia^{1,2}, Jun Ma¹, Zhaofeng Zhuang¹, Guangmin Zhou¹*, Hui-Ming Cheng^{3,4*}

¹ *Tsinghua-Berkeley Shenzhen Institute & Tsinghua Shenzhen International Graduate School, Tsinghua University, Shenzhen 518055, China*

² *Frontiers Science Center for Transformative Molecules, School of Chemistry and Chemical Engineering, Shanghai Jiao Tong University, Shanghai 200240, China*

³ *Faculty of Materials Science and Engineering / Institute of Technology for Carbon Neutrality, Shenzhen Institute of Advanced Technology, Chinese Academy of Science, Shenzhen 518055, China* ⁴ Shenyang National Laboratory for Materials Science, Institute of Metal Research, Chinese *Academy of Sciences, Shenyang 110016, China*

* Corresponding authors: Zheng Liang (Email: liangzheng06@sjtu.edu.cn); Guangmin Zhou (Email: guangminzhou@sz.tsinghua.edu.cn); Hui-Ming Cheng (Email: cheng@imr.ac.cn) # These authors contributed equally to this work.

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Supplementary Text Supplementary Fig. 1 to Fig. 30 Supplementary Table 1 to Table 19

Cathode materials

Anode materials

Supplementary Fig. 1 Recycling procedure of spent LIBs. 18650 degraded LIBs (1.2 Ah) were manually disassembled in a fume cupboard and the cathodes, anodes, and separators removed. The cathode sheets were immersed in water and the spent powder could then be easily separated from the Al foil due to its water-based binder. For the anode sheets, spent graphite powder was also collected during the same operation.

Supplementary Fig. 2 XRD spectra of S-LFP, R-LFP-LiOH, R-LFP-Li₂CO₃, and R-LFP-Li₂DHBN.

Supplementary Fig. 3 XPS survey of S-LFP, R-LFP-LiOH, R-LFP-Li₂CO₃, and R-LFP-Li₂DHBN.

Supplementary Fig. 4 SEM images of degraded LFP cathode materials at **a** low and **b** high resolutions.

Supplementary Fig. 5 The pictures during Li₂DHBN synthesis process. **a** A yellow solution before filtration. **b, c** The final Li2DHBN precipitate after filtration and dry.

Supplementary Fig. 6 a The pictures of Li2DHBN before and after heat treatment. **b** XRD spectra of Li2DHBN after heat treatment.

Supplementary Fig. 7 a TG-DTA, **b** TG-IR, and **c** IR contour map of the mixture of S-LFP powder and Li₂DHBN. To simulate our experimental process, the mixture of S-LFP powder and Li₂DHBN was also used for TR-FTIR measurements. The optimum weight of organic lithium salt is 5 wt%. The peaks are not obvious from the IR contour map due to the small quantity of Li₂DHBN. TG-DTA results show the same decomposition process as **Fig. 1e**.

Supplementary Fig. 8 TEM images and corresponding enlarged figures of **a, b** S-LFP, **c, d** R-LFP-Li2CO3, and **e, f** R-LFP-Li2DHBN.

Supplementary Fig. 9 Microstructure characterization of R-LFP-Li2CO³ cathode. a TEM image, **b, f** enlarged figures, **c, g** SAED images from FFT results, **d, h** inverse FFT results, and **e, i** the corresponding line profiles in Supplementary Figs. 9d and 9h.

Supplementary Fig. 10 EDS elemental maps of **a** S-LFP, **b** R-LFP-Li2CO³ and **c** R-LFP-Li2DHBN.

Supplementary Fig. 11 EDS energy spectra of **a** S-LFP, **b** R-LFP-Li₂CO₃ and **c** R-LFP-Li₂DHBN.

Supplementary Fig. 12 The initial three CV curves of **a** S-LFP, **b** R-LFP-LiOH, **c** R-LFP-Li2CO3, **d** R-LFP-Li2DHBN.

Supplementary Fig. 13 CV curves at different scan rates of **a** S-LFP, **b** R-LFP-LiOH, and **c** R-LFP- $Li₂CO₃$.

Supplementary Fig. 14 GITT curves during the first cycle of S-LFP, R-LFP-LiOH, R-LFP-Li₂CO₃, and R-LFP-Li2DHBN.

The Li-ion diffusion rate calculated from the GITT curve is based on the following formula according to Fick's second law of diffusion^{1, 2, 3}:

D=4/ $\pi\tau$ ($n_M V_M/S$)²($\Delta E_S/\Delta E_t$)²

where τ is the duration of the current pulse, n_M is the number of moles, V_M is the molar volume of the electrode, S is the electrode-electrolyte contact area, and ΔE_s and ΔE_t are the changes in the steady state potential and the total change during the current flux by deducting the IR drop, respectively. In our experiments, $\tau = 1800$ s, $n_M = m/M_{LFP}$, $M_{LFP} = 157.76$ g mol⁻¹, $V_M = 20.5$ cm³ mol⁻¹, $S = 1.13$ cm³.

Supplementary Fig. 15 GITT profiles for the discharge/charge process (red curves) and diffusion coefficients (blue curves) of **a** R-LFP-LiOH, **b** R-LFP- Li₂CO₃, and **c** R-LFP-Li₂DHBN.

Supplementary Fig. 16 The electrochemical performance obtained from different usages of Li2DHBN. **a** Charge-discharge curves, **b** rate capabilities, **c** cycling performance of R-LFP-Li2DHBN.

Supplementary Fig. 17 The electrochemical performance obtained at different temperatures. **a** Charge-discharge curves, **b** rate capabilities, **c** cycling performance of R-LFP-Li₂DHBN.

Supplementary Fig. 18 a The cycling performance at 1 C rate and **b** the corresponding capacity retentions of S-LFP, R-LFP-LiOH, R-LFP- Li₂CO₃, and R-LFP-Li₂DHBN.

Supplementary Fig. 19 a The cycling performance at 10 C rate and **b** the corresponding capacity retentions of R-LFP-LiOH, R-LFP- Li₂CO₃, and R-LFP-Li₂DHBN.

Supplementary Fig. 20 Demonstration of the versatility of Li2DHBN. The cycling performance and charge-discharge profiles at a rate of 0.5 C of **a, b** R-NCM and **c, d** R-LCO.

To demonstrate the versatility of the organic lithium salt, S-LCO and S-NCM cathodes were also investigated under the optimal experimental conditions. As depicted in **Supplementary Fig. 20**, the R-LCO sample has a specific discharge capacity of 125 mAh g^{-1} after 250 cycles with a high retention of 83%. In comparison, the S-LCO could only retain a capacity of 90 mAh g^{-1} which decreased sharply after 200 cycles. For the R-NCM sample, the improved specific capacity reached about 120 mAh g^{-1} and retained 84% of the initial value. The original S-NCM sample was almost completely degraded after long cycling. It is concluded that the Li₂DHBN can be used to restore different types of spent LIB cathodes with different degrees of degradation, thus providing a competitive lithium supplement for future direct regeneration technology.

Supplementary Fig. 21 The impedance spectra of **a** R-LFP-Li₂CO₃ and **b** R-LFP-LiOH collected during the first cycle.

Supplementary Fig. 22 a STEM image, **b** O K-edge and Fe L-edge, and **c** Li K-edge EELS of S-LFP particle-1.

Supplementary Fig. 23 a STEM image, **b** O K-edge and Fe L-edge, and **c** Li K-edge EELS of S-LFP particle-1.

Supplementary Fig. 24 a STEM image, **b** O K-edge and Fe L-edge, and **c** Li K-edge EELS of S-LFP particle-2.

Supplementary Fig. 25 a STEM image, **b** O K-edge and Fe L-edge, and **c** Li K-edge EELS of S-LFP particle-3.

Supplementary Fig. 26 a STEM image, **b** O K-edge and Fe L-edge, and **c** Li K-edge EELS of R-LFP.

Supplementary Fig. 27 Pie chart of the % costs involved in direct recovery.

Supplementary Fig. 28 Pie charts of the % revenues obtained using **a** hydro-recovery and **b** direct recovery.

Supplementary Fig. 29 a Total energy consumption and **b** GHG emissions of recycling 1 kg spent LFP batteries by pyro-, hydro-, and direct recovery.

Supplementary Fig. 30 a Cost, **b** revenue, and **c** profit recycling 1 kg spent LFP batteries by pyro-, hydro-, and direct recovery.

The total costs of pyro-, hydro-, and direct recycling are \$1.99, \$1.52, and \$1.37 per kg of cells, respectively (**Supplementary Table 10 and Supplementary Fig. 30a**). Raw materials cost is mainly responsible for the manufacturing cost in direct recycling due to the high price of lithium salt. The recycled Al, Cu, graphite, and LFP is assumed to be sold to compensate some cost of the recycling processes (**Supplementary Table 11**). Notably, the recycled LFP is mainly attributed to the total revenue for direct recycling, which is higher than pyro- and hydro- recycling (**Supplementary Fig. 30b**). Therefore, the profits of pyro-, hydro-, and direct recycling are respectively \$-1.12, \$-0.59, and \$1.28 per kg of cells (**Supplementary Fig. 30c**).

Supplementary Table 1 The degraded LIBs used in the recovery process and the corresponding basic parameters.

	Element content (wt%)			Molar ratio	
	Li	P	Fe	Li/P	Li/Fe
C-LFP	4.44	18.48	33.27	1.07	1.07
R-LFP-Li ₂ DHBN	4.14	18.2	30.98	1.01	1.07
R -LFP-Li ₂ CO ₃	4.41	18.11	32.36	1.08	1.09
R-LFP-LiOH	4.46	18.41	32.14	1.08	1.11
S-LFP	3.84	18.5	32.26	0.92	0.98

Supplementary Table 2 Element content and molar ratio of C-LFP, R-LFP and S-LFP samples based on ICP-OES results. (Note: C-LFP represents a commercial LiFePO₄ cathode)

Supplementary Table 3 Summary of direct regeneration methods and their performance of LFP cathodes. (With annealing: No. 1-10; without annealing: No. 11-16; this work: No. 17)

SOC/DOD	$R_0(\Omega)$	$R_{ct}(\Omega)$	σ (Ω cm ² s ^{-1/2})
OCV	1.167	47.78	33.43
$C-2.5V$	1.222	57.18	29.52
$C-3.4V$	1.207	52.67	42.42
$C-3.4V$	1.223	44.01	36.79
$C-3.5V$	1.126	38.52	45.26
$C-3.6V$	1.216	35.7	29.68
$C-4.0V$	1.23	32.92	18.67
$C-4.3V$	1.214	33.99	19.80
$D-4.0V$	1.205	36.48	21.35
D-3.4V	1.221	35.71	34.77
$D-3.3V$	1.232	44.05	42.25
$D-3.2V$	1.237	44.32	41.26
$D-3.0V$	1.25	43.01	45.18
$D-2.5V$	1.245	43.6	41.73

Supplementary Table 4 Fitting result of equivalent circuit model for impedance parameters at different state of S-LFP sample. (OCV-open circuit voltage; C-charge; D-discharge)

SOC/DOD	$R_0(\Omega)$	$R_{ct}(\Omega)$	σ (Ω cm ² s ^{-1/2})
OCV	4.697	62.33	60.54
$C-2.5V$	4.363	72.34	63.63
$C-3.4V$	4.315	70.16	62.30
$C-3.4V$	4.215	60.28	58.66
$C-3.5V$	4.375	22.2	45.08
$C-3.6V$	4.234	21.49	66.73
$C-4.0V$	4.205	20.36	26.95
$C-4.3V$	4.203	20.11	27.69
$D-4.0V$	4.221	21.05	27.40
D-3.4V	4.208	20.53	12.64
$D-3.3V$	4.309	27.07	71.92
$D-3.2V$	4.325	27.61	70.38
$D-3.0V$	4.328	28.07	73.22
$D-2.5V$	4.287	27.81	82.19

Supplementary Table 5 Fitting result of equivalent circuit model for impedance parameters at different state of R-LFP-Li2DHBN sample. (OCV-open circuit voltage; C-charge; D-discharge)

Supplementary Table 6 Structural parameters obtained from Rietveld refinement of the X-ray diffraction pattern of S-LFP. **Phase 1 LiFePO4**: Space group: *Pnma*, *a* = 10.32823 Å, *b* = 6.00687 Å, $c = 4.69310 \text{ Å}, V = 291.161 \text{ Å}^3, \ \alpha = \beta = \gamma = 90^\circ, \text{ Fraction: } 78.70\%$. **Phase 2 FePO**4: Space group: *Pnma*, *a* = 5.79049 Å, *b* = 9.81996 Å, *c* = 4.78393 Å, *V* = 272.025 Å³, *α* = *β* = *γ* = 90°, Fraction: 21.30%.

Supplementary Table 7 Structural parameters obtained from Rietveld refinement of the X-ray diffraction pattern of R-LFP-Li₂DHBN. **Phase LiFePO**4: Space group: *Pnma*, $a = 10.32347 \text{ Å}$, $b =$ 6.00249 Å, $c = 4.69709$ Å, $V = 291.063$ Å³, $\alpha = \beta = \gamma = 90^{\circ}$, Fraction: $100(\pm 0.77)$ %.

Atoms	Site	Wyckoff positions			Occupancy
Li1	4a	$\overline{0}$	$\overline{0}$	$\overline{0}$	0.988
Fe ₂	4a	$\overline{0}$	$\overline{0}$	$\overline{0}$	0.012
Fe1	4c	0.28291	0.25000	0.97378	0.988
Li2	4c	0.28291	0.25000	0.97378	0.012
P ₁	4c	0.09857	0.25000	0.42966	$\mathbf{1}$
O ₁	4c	0.08372	0.25000	0.73929	$\mathbf{1}$
O ₂	4c	0.44779	0.25000	0.25914	$\mathbf{1}$
O ₃	8d	0.15309	0.04042	0.26696	1

	Pyro-	Hydro-	Direct
Ammonium Hydroxide	NR	0.031	NR
Hydrochloric Acid	0.21	0.012	NR
Hydrogen Peroxide	0.06	0.366	NR
Sodium Hydroxide	NR	0.561	NR
Limestone	0.30	NR	NR
Sand	0.15	NR	NR
Sulfuric Acid	NR	1.08	NR
Soda Ash	NR	0.02	NR
Lithium Hydroxide	NR	NR	0.047
Citric Acid	NR	NR	NR
Lithium Carbonate	NR	NR	0.030
Li ₂ DHBN	NR	NR	0.093

Supplementary Table 8 Materials requirements (kg) to recycle 1 kg of spent batteries through different recycling technologies. (NR = Not Required)

Supplementary Table 9 Life-cycle environmental impacts of different recycling methods.

Supplementary Table 10 Manufacturing cost details for different recycling processes per year (10,000 tons of spent batteries).

Supplementary Table 11 Value of recycled materials (\$/kg).

Original data of techno-economic analysis

Supplementary Table 12 Basic data.

 1 \$ = 6.698 ¥ (Update time: 2022/7/5). ② Data Sources: SMM (https://www.smm.cn/), 100PPI (http://www.100ppi.com/ppi/), BDB (http://sz.bendibao.com/), 51wctt (https://mp.weixin.qq.com/s/AoXhIwQzLquIL_Csrkw7lw).

Supplementary Table 13 Hydro- recovery cost analysis.

 $\overline{0}$ In Supplementary Table 13, we calculated the cost per one ton of recycled cathode materials. The recycle process can be divided into three steps: disassembly of degraded battery, seperation of cathode active material, extraction of lithium.

 $\oslash\,$ We assume that the failure degree of spent LFP batterry is consistent (Li $_{0.8}$ FePO $_4$) based on Hydro- and direct recovery.

Supplementary Table 14 Direct recovery cost analysis.

material, regeneration of LFP material.

 $\oslash\,$ We assume that the failure degree of spent LFP batterry is consistent (Li $_{0.8}$ FePO $_4$) based on Hydro- and direct recovery.

Supplementary Table 15 Hydro- recovery revenue analysis.

subtotal (¥) 32314.9741

Note: \odot We assume that the failure degree of spent LFP batterry is consistent (Li_{0.8}FePO₄) based on Hydro- and direct recovery. \odot The proportion of each compenent is 27% of cathode material, 13% of graphite, 6% of Al foil, 10% of Cu foil, 3% of separator, 16% of electrolyte, and 27% of shell (Ref: https://doi.org/10.1016/j.est.2020.102217). ③ The value of Li₂CO₃, FePO₄, and graphite is calculated based on the real market price from SMM. ④ The value of separator, electrolyte and shell is hard to assess in real process, therefore, these components are not included in our revenue analysis.

Supplementary Table 16 Direct recovery revenue analysis.

Note: ① We assume that the failure degree of spent LFP batterry is consistent (Li_{0.8}FePO₄) based on Hydro- and direct recovery. ② The proportion of each compenent is 27% of cathode material, 13% of graphite, 6% of Al foil, 10% of Cu foil, 3% of separator, 16% of electrolyte, and 27% of shell (Ref: https://doi.org/10.1016/j.est.2020.102217). ③ The value of regenerated LiFePO₄ is calculated based on the real market price from SMM. ④The value of separator, electrolyte and shell is hard to assess in real process, therefore, these compenents are not included in our revenue analysis.

Supplementary Table 17 Hydro- recovery cost results.

Supplementary Table 18 Direct recovery cost results.

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